

**M.Sc. Thesis**

*Cranfield*  
UNIVERSITY

**School of Engineering  
Department of Power and Propulsion**

# **Emissions Estimation from Industrial Gas Turbine Combustors**

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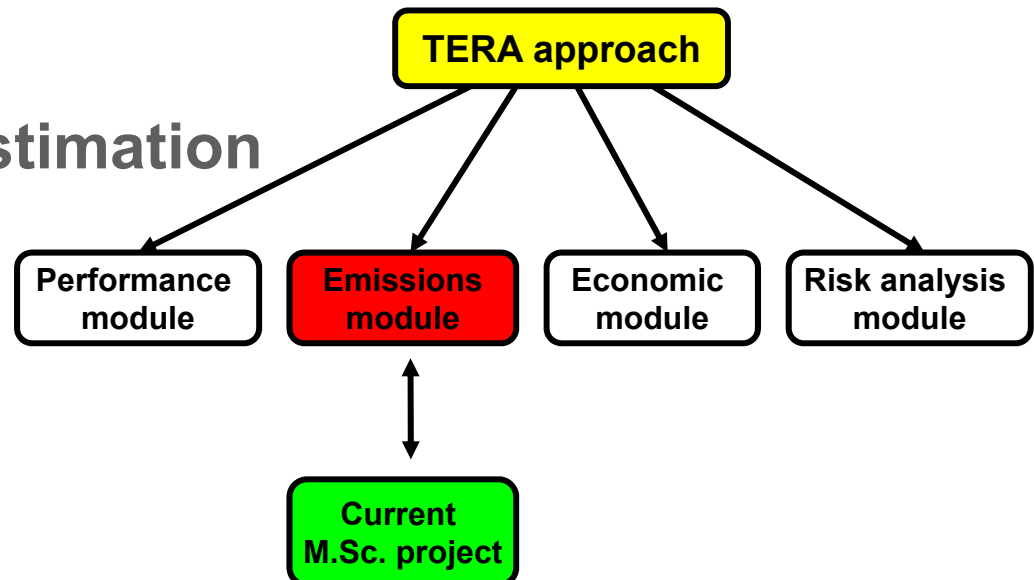
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# 1. T.E.R.A. approach

## T. E. R. A.

### Techno - Economical Risk Analysis

- ❖ Investigation of advanced low carbon power cycles
- ❖ Performance analysis
- ❖ Environmental impact estimation
- ❖ Economic evaluation
- ❖ Risk analysis



## 2. Project objectives

**Development of an algorithm aimed to estimate the pollutant emissions trends from industrial gas turbine combustors**



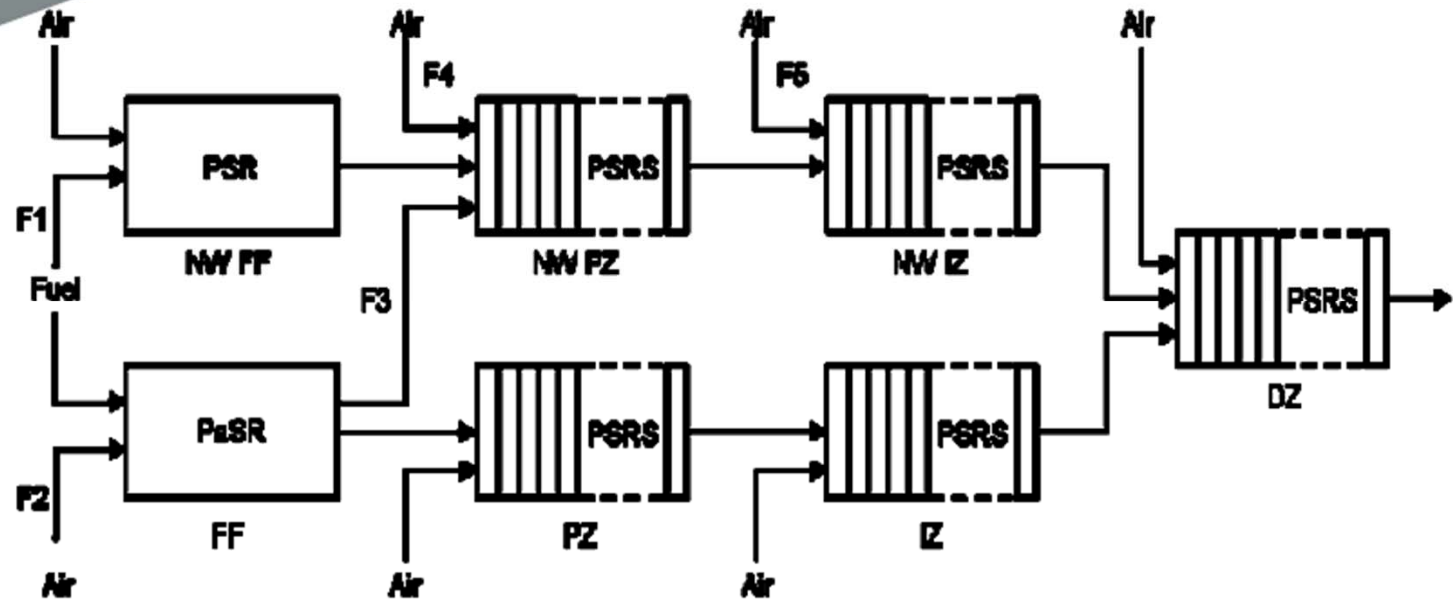
**Application to the T.E.R.A. selected cycles (particular gas turbine)**



**Investigation of the estimative potential of the model (parametric analysis)**

# 3. Algorithm development

## Reactors arrangement



Reactors used:

- ✓ Perfectly stirred reactors (PSR)
- ✓ Series of perfectly stirred reactors (PSRS)
- ✓ Partially stirred reactors (PaSR)

F1	0.20
F2	0.65
F3	0.25
F4	0.20
F5	0.20

# 3. Algorithm development

## Empirical correlations

**NOx**  $\leftarrow$  Thermal NO:  $\frac{dY_{NO}}{dt} = \frac{2M_{NO}}{\rho} (1 - \alpha^2) \left[ \frac{R_1}{1 + aK_1} + \frac{R_6}{1 + K_2} \right]$

**NOx**  $\leftarrow$  Prompt NO:  $\frac{dY_{NO}}{dt} = \left( \frac{M_{NO}}{\rho} \right) f_{pr} k'_{pr} [O_2]_e^a [N_2]_e \times [CH_4] \exp\left(\frac{-36499.507}{T}\right)$

**CO**  $\frac{dY_{CO}}{dt} = -k_{7f} \left( \frac{M_{CO}}{\rho} \right) [OH]_e \times \left[ 1 + \frac{[CO]_e}{[CO_2]_e} \right] ([CO] - [CO]_e)$

**UHC**  $\frac{dY_{CH_4}}{dt} = -10^{10.2} \left( \frac{M_{CH_4}}{\rho} \right) e^{\left(\frac{-48400}{RT}\right)} [Y_{CH_4}]^{0.7} [Y_{O_2}]^{0.8}$

**Soot/smoke**  $\leftarrow$  Formation:  $S_f = 1.4887 \times 10^{-4} \left( \frac{\phi FAR_s}{\dot{m}_a T} \right) P^2 \times (18 - H_{cont})^{1.5} \left( \frac{\dot{m}_{g_i}}{\rho_{soot}} \right)$

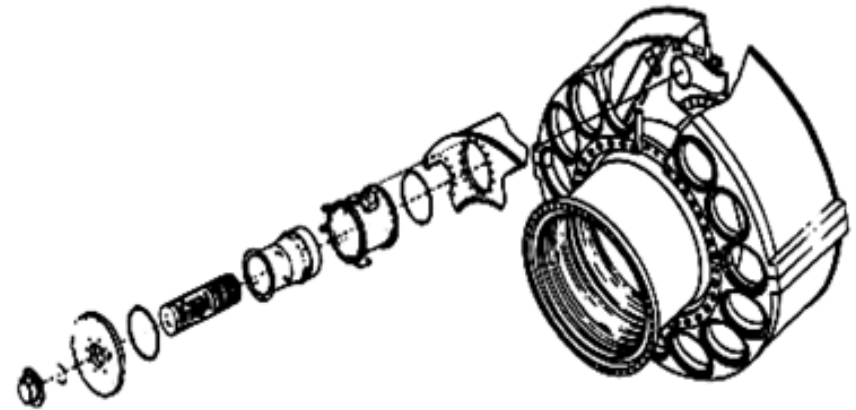
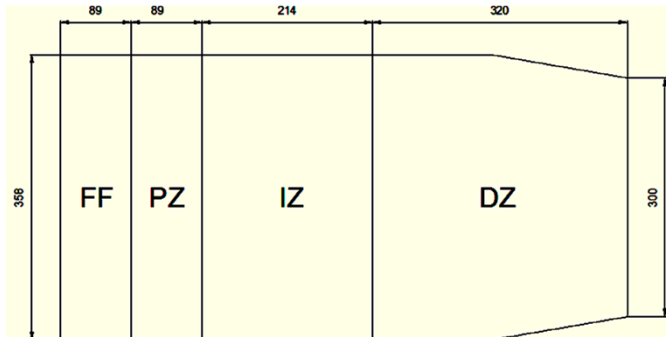
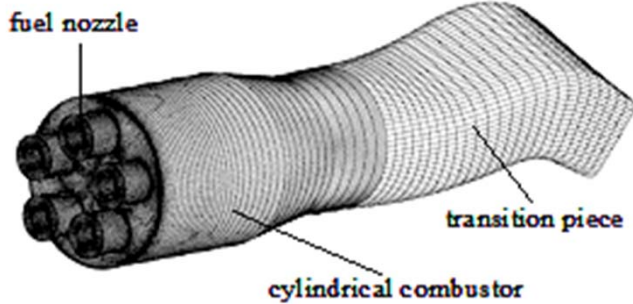
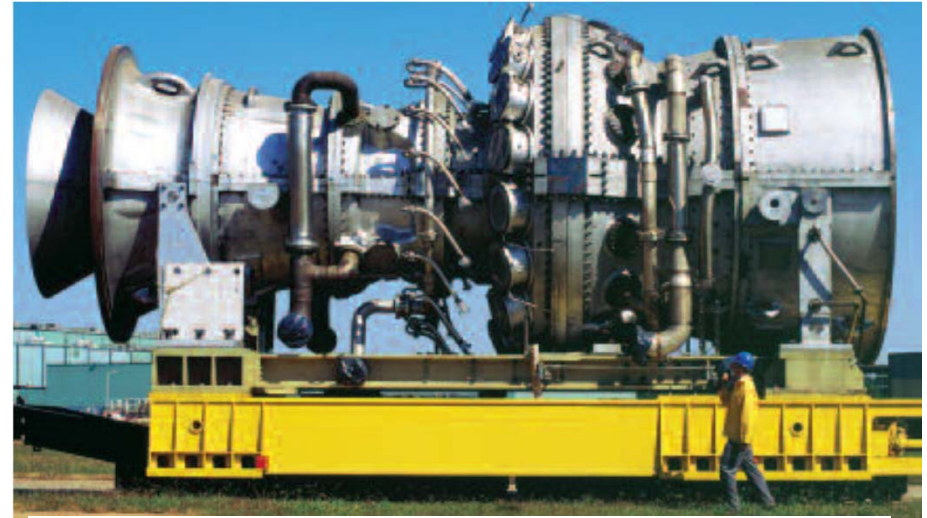
**Soot/smoke**  $\leftarrow$  Oxidation:  $W_{O_2} = \pi^{1/3} \cdot 6^{2/3} \cdot \phi^{2/3} \cdot N^{1/3} \cdot W'_{O_2} / \rho_{soot}$

**Soot/smoke**  $\leftarrow$  Oxidation:  $W_{OH} = 10.14 \cdot \theta \cdot \phi^{2/3} \cdot N^{1/3} \cdot X_{OH} \cdot T^{1/2}$



# 3. Algorithm development

## Simulated engine



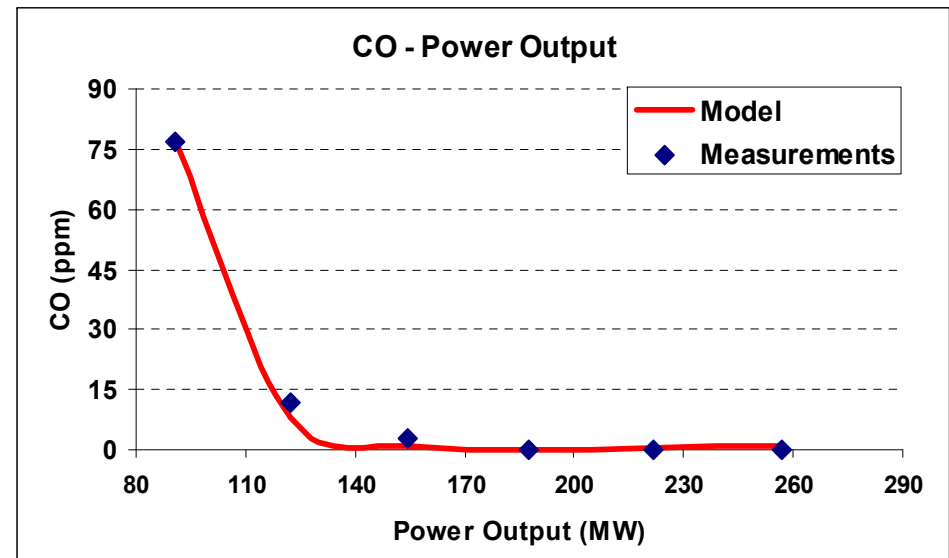
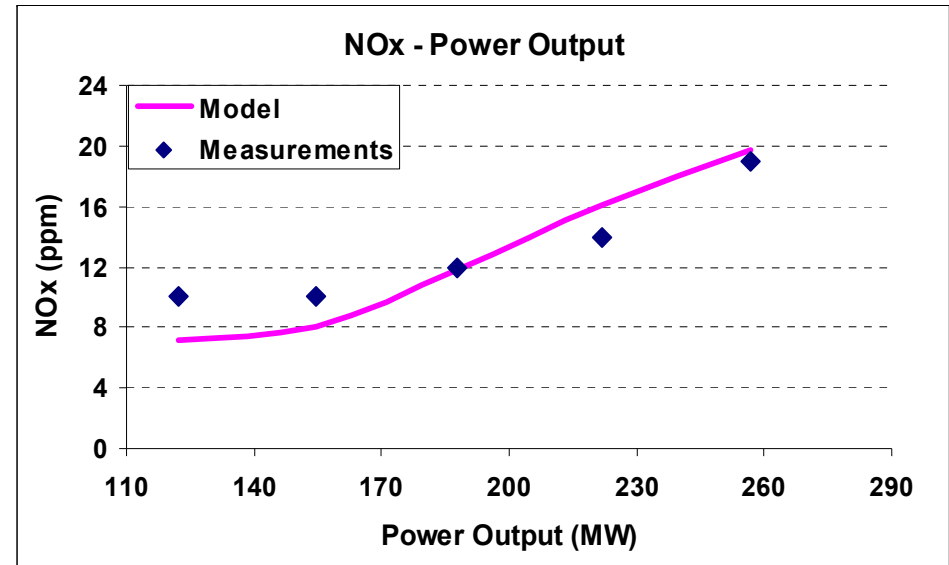
- 18 combustors
- DLN-2+ technology
- 2 operational modes



# 4. Model results for natural gas

## Estimated VS Measured

- Only the second (premixed) stage was simulated
- There is an almost exponential relationship between emissions and power output
- CO emissions were slightly underestimated throughout the covered power range
- Both emissions trends were sufficiently reproduced



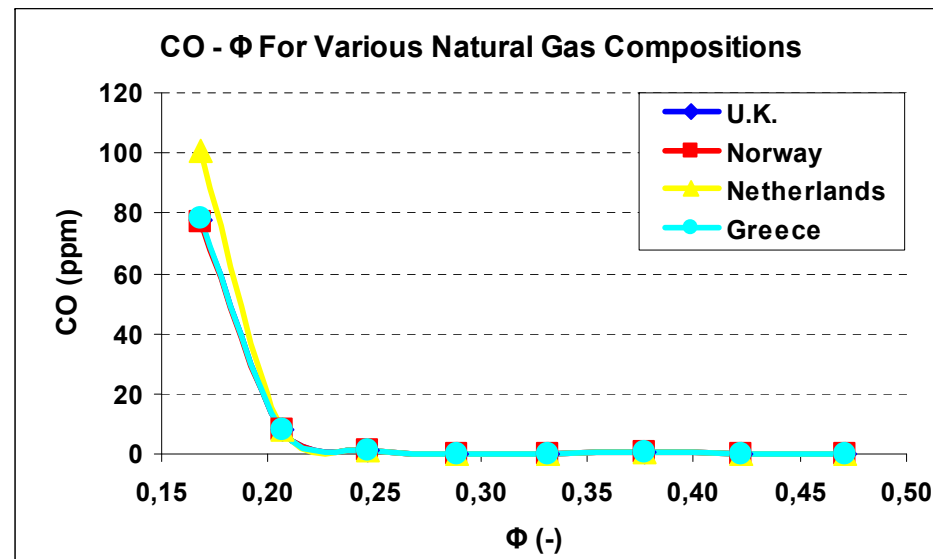
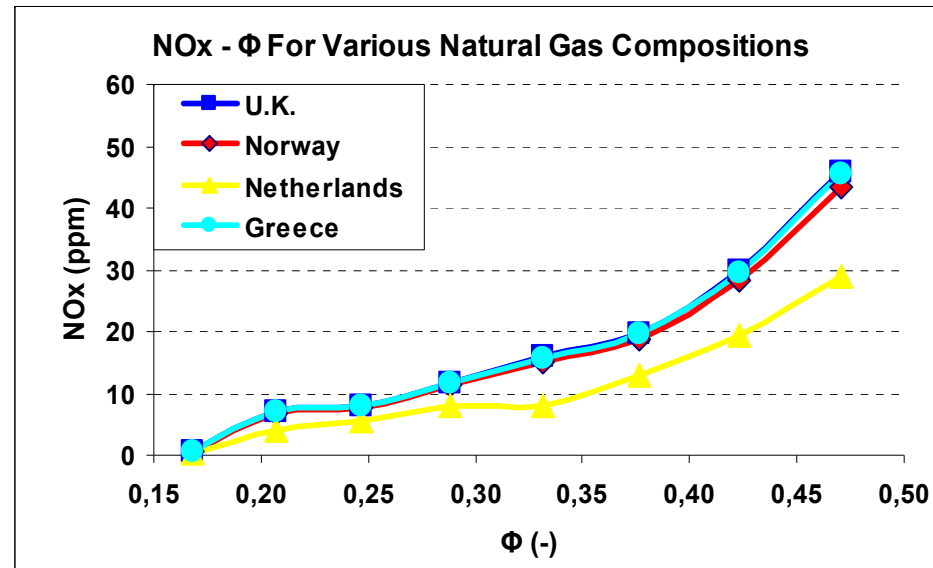
# 4. Model results for natural gas

## Fuel composition impact

Lowest value

	NG used in U.K.	NG used in Greece	NG used in Norway	NG used In Netherlands
CH <sub>4</sub>	0.8620	0.9322	0.7812	0.6998
C <sub>2</sub> H <sub>6</sub>	0.1080	0.0305	0.0993	0.0463
C <sub>3</sub> H <sub>8</sub>	-	0.0128	0.0485	0.0090
C <sub>4</sub> H <sub>10</sub>	-	0.0081	0.0160	0.0085
N <sub>2</sub>	0.0250	0.0137	0.0308	0.2154
CO <sub>2</sub>	0.0050	0.0027	0.0242	0.0210
Total	1.0000	1.0000	1.0000	1.0000

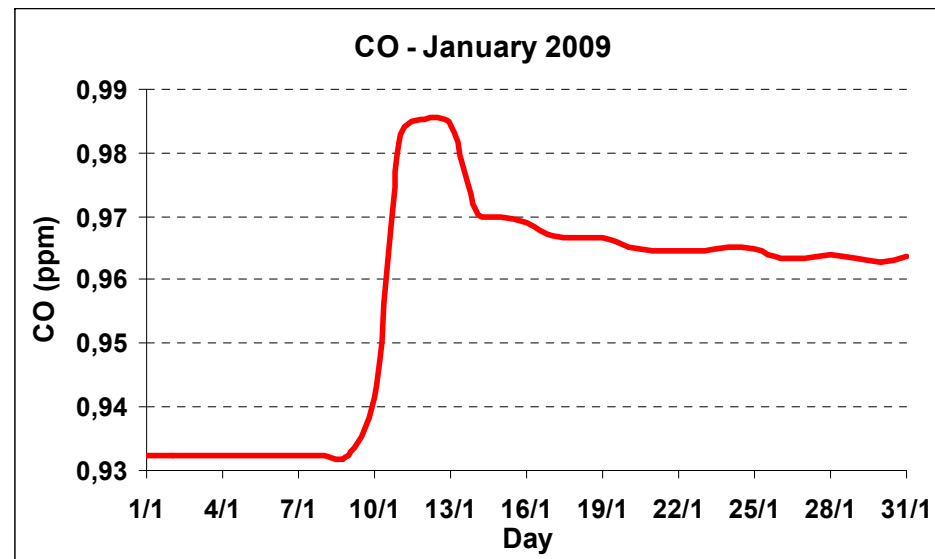
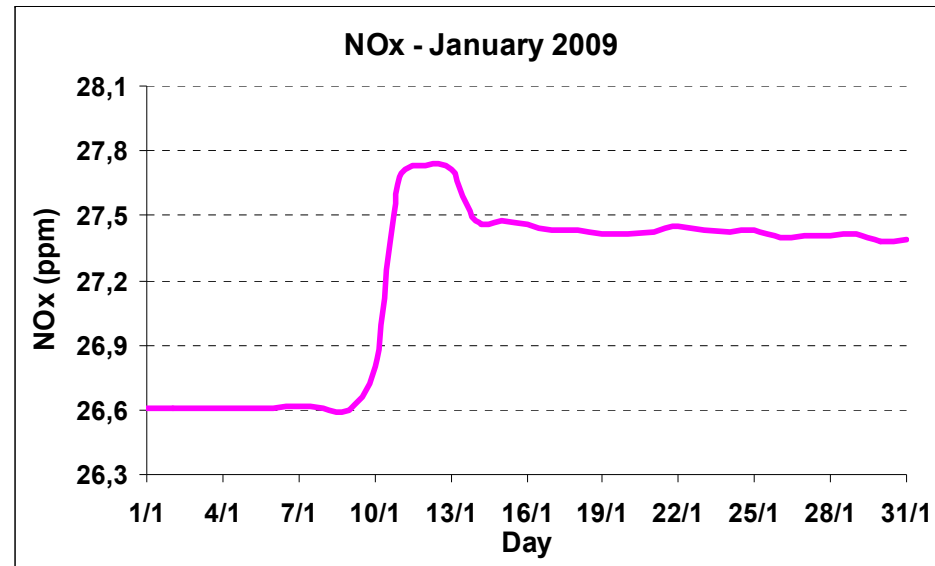
NG used in Netherlands is expected to produce lower NOx but higher CO emissions than the rest NGs



# 4. Model results for natural gas

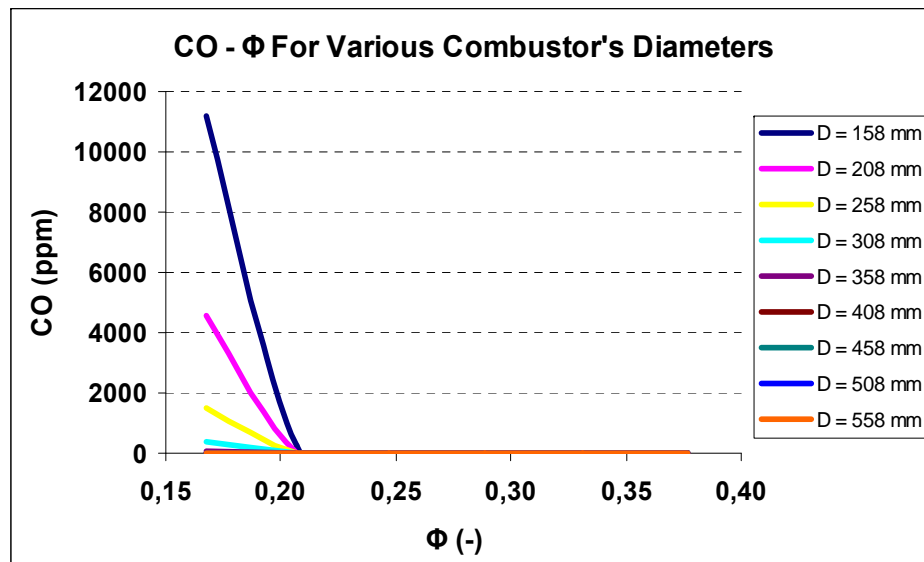
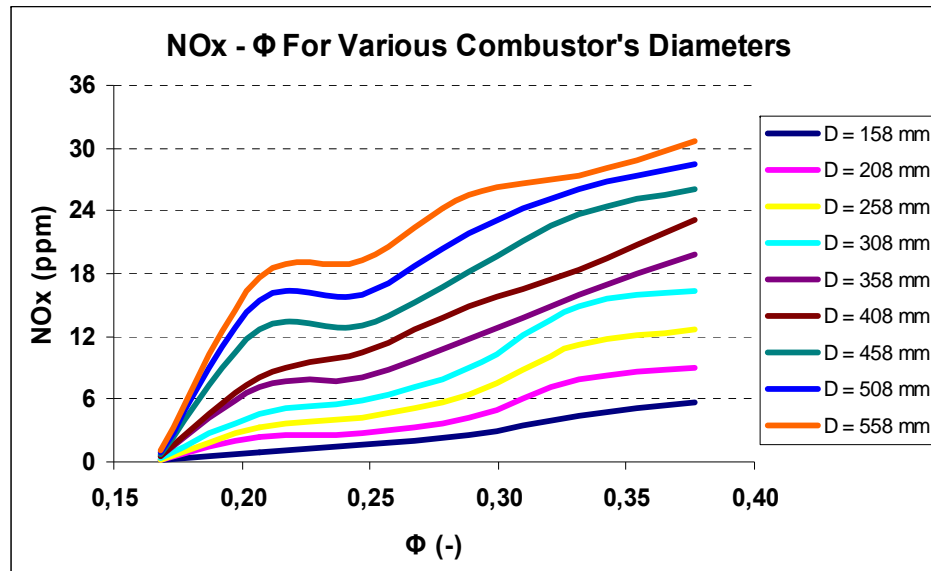
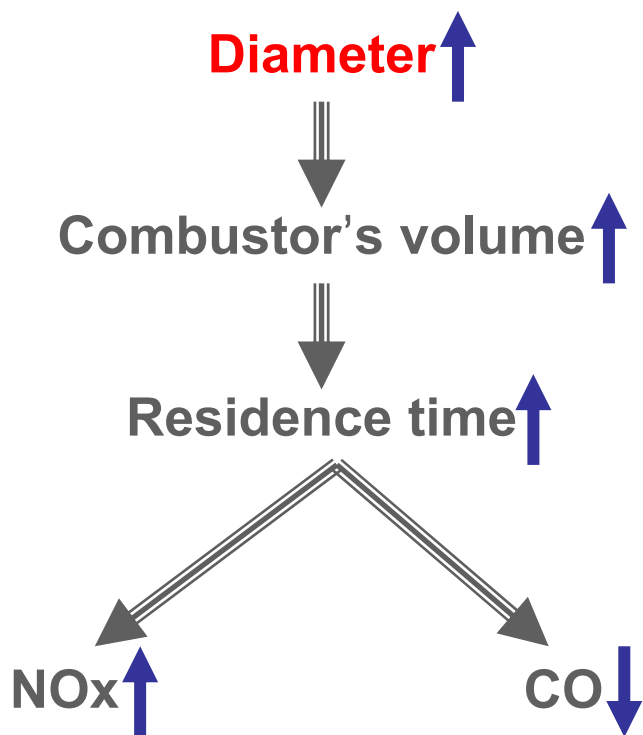
- The composition of natural gas is not steady even within a day
- Both NOx and CO emissions vary daily due to the fuel composition change
- 1.34% rise in fuel hydrocarbon content results in 4.24% and 5.69% increase in NOx and CO emissions respectively

## Daily emissions results



# 4. Model results for natural gas

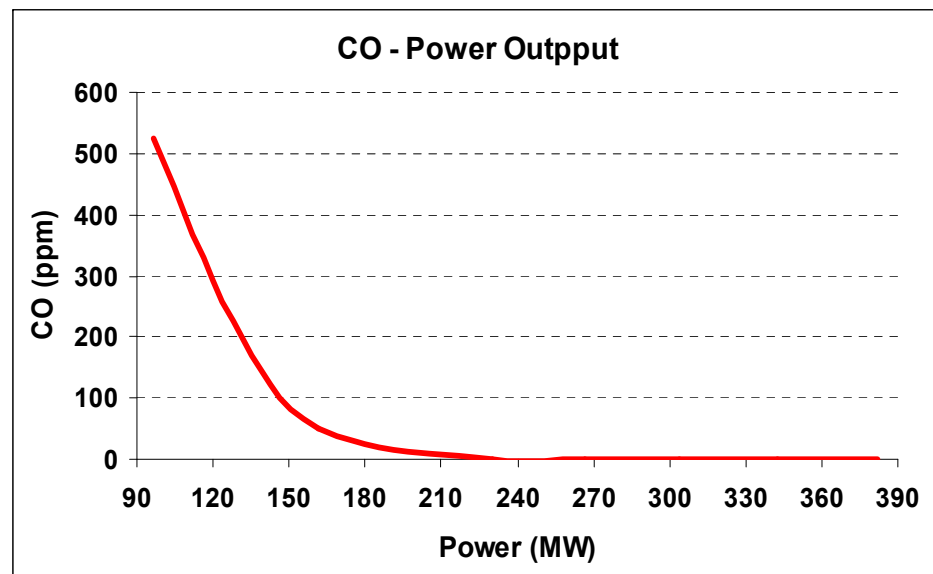
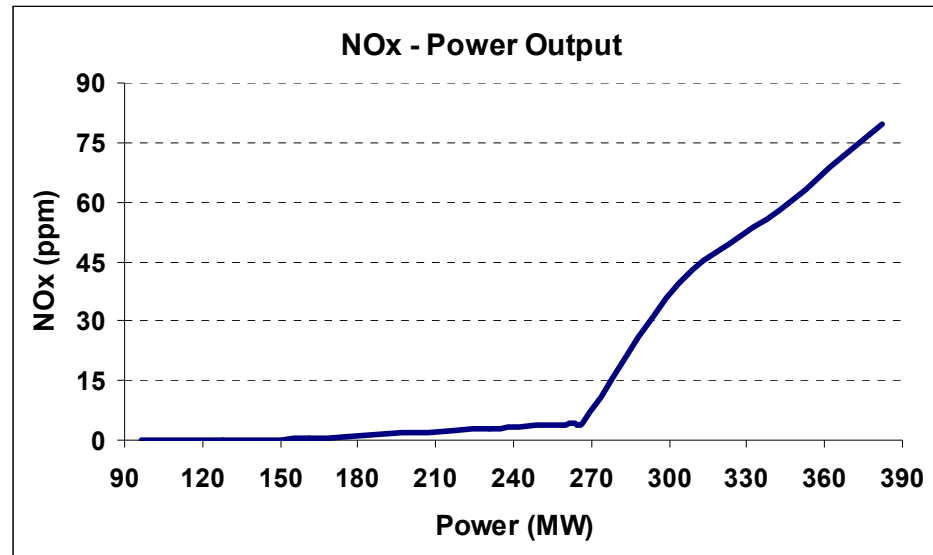
## Combustor's size impact



# 5. Model results for syngas

- ❖ Again, only the second stage of the engine was simulated
- ❖ After design point (266MW) there is a dramatic increase in NOx emissions
- ❖ CO emissions are expected to be high during part load operation (load < 180MW)
- ❖ The low emissions area is estimated between 240MW and design point

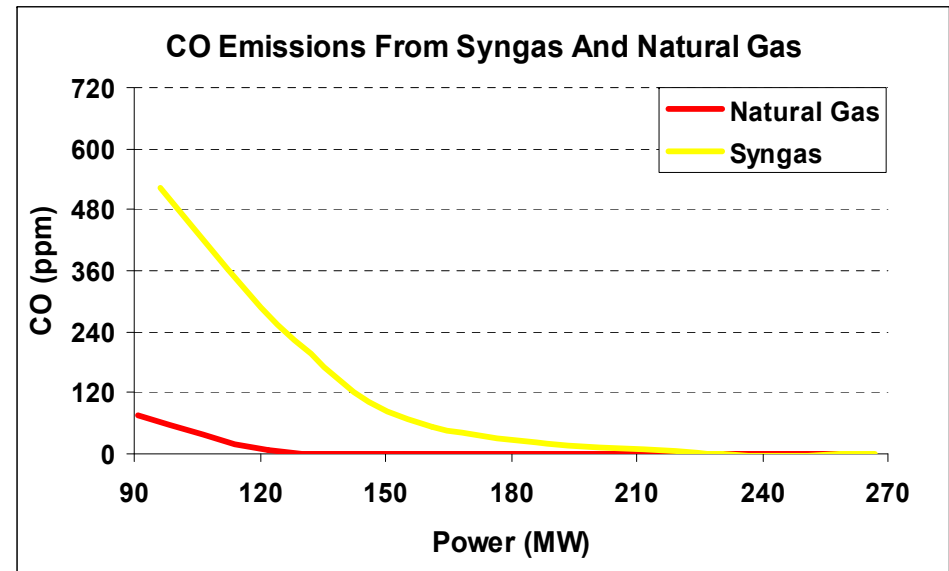
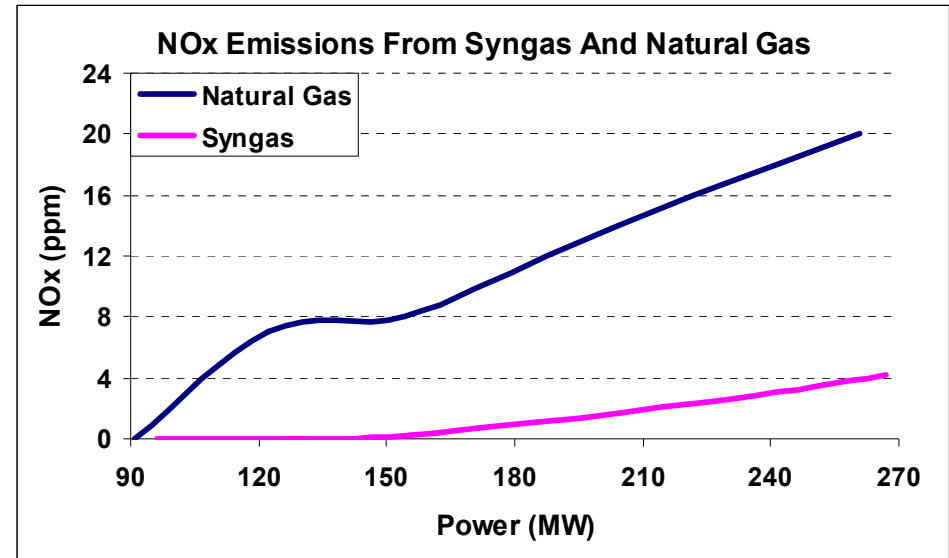
## Emissions – Power



# 5. Model results for syngas

- ✓ Close to DP, if the engine is fed with syngas, it is expected to produce lower NOx and similar CO emissions with NG
- ✓ During part load operation NG is favored since it will produce lower CO emissions than syngas (for the same engine)
- ✓ Syngas mass flow = almost 5 x NG mass flow (for the same power output), due to the lower LHV of syngas

## NG VS Syngas



# 5. Model results for syngas

## Parametric analysis

**Highest values**

		Natural Gas		Syngas	
	Parameter Range	NO <sub>x</sub>	CO	NO <sub>x</sub>	CO
Fuel Inlet Temperature	273 – 493 K	9.34%	-12.59%	61.45%	-12.5%
Ambient Temperature	263 – 318 K	5.97%	-44.07%	83.45%	-8.18%
Ambient Relative Humidity	0 – 100%	-9.34%	12.59%	-5.40%	3.42%

- The change of the parameters is expected to produce similar changes in emissions trends of both fuels (either increasing or decreasing)
- The variation of ambient temperature is estimated to cause the highest change in emissions production of both fuels
- The ambient relative humidity has the lowest impact in emissions production of both fuels

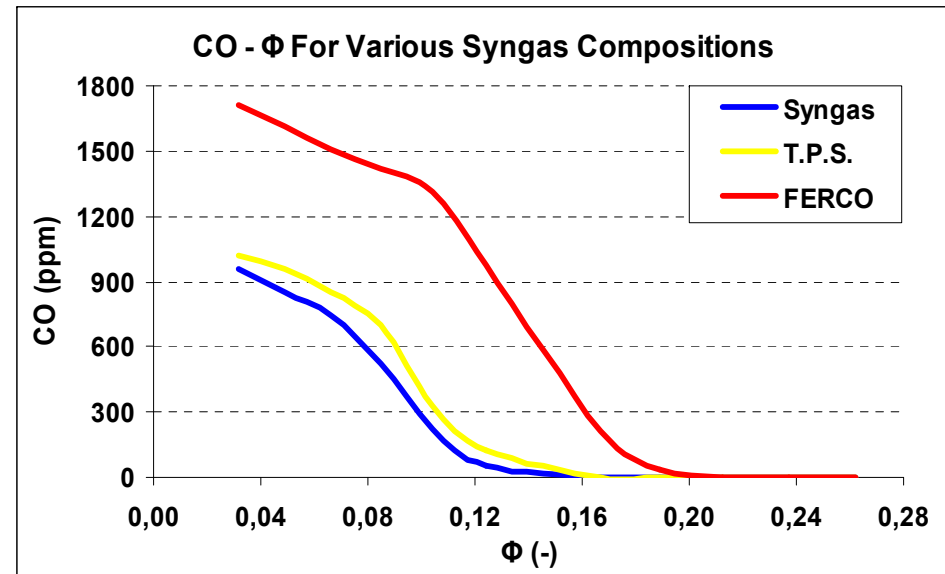
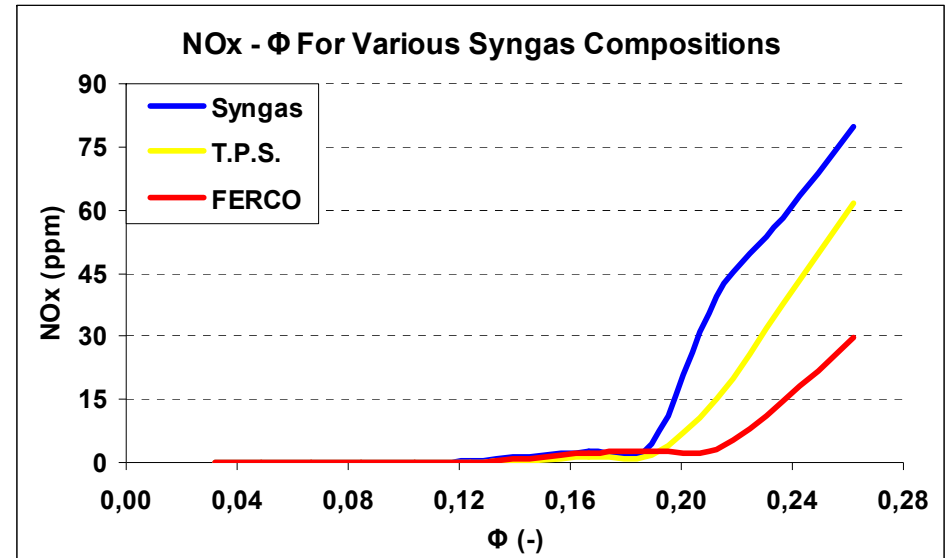
# 5. Model results for syngas

## Fuel composition impact

Highest values

	SYNGAS	TPS	FERCO
CH <sub>4</sub>	0.0260	0.0186	0.1118
C <sub>2</sub> H <sub>6</sub>	-	-	0.0094
C <sub>2</sub> H <sub>4</sub>	-	0.0108	0.0639
N <sub>2</sub>	0.8240	0.4977	-
H <sub>2</sub> O	0.0140	0.0070	-
H <sub>2</sub>	0.0740	0.0117	0.0198
CO	0.0030	0.2163	0.5553
CO <sub>2</sub>	0.0590	0.2379	0.2398
Total	1.0000	1.0000	1.0000

FERCO syngas is expected to produce the lowest NOx but the highest CO emissions





## 6. Conclusions

- ❖ Emissions trends were sufficiently reproduced
- ❖ Estimated emissions were in agreement with the measured data for the natural gas case
- ❖ The results of parametric analysis were (more or less) in accordance with the established theory
- ❖ Air/fuel temperature, ambient conditions, fuel composition and the size of combustor strongly affect the emissions
- ❖ From an emissions point of view, syngas could substitute natural gas in the particular engine

# 7. Recommendations

- **Simulation of a different engine  
– further validation of the model**
- **Use of more accurate geometry data for the combustor**
- **By using Variflow results an improved version of the model should be able to estimate the emissions trends for the entire power range of the engine**
- **Adaptation of a different reactors arrangement**
- **Use of different semi-empirical equations**